

82-1; 1,3,5-trichlorobenzene, 108-70-3; 1,2,3,4-tetrachlorobenzene, 634-66-2; 1,2,3,5-tetrachlorobenzene, 634-90-2; 1,2,4,5-tetrachlorobenzene, 95-94-3; pentachlorobenzene, 608-93-5; hexachlorobenzene, 118-74-1; 2-chlorobiphenyl, 2051-60-7; 2,5-dichlorobiphenyl, 34883-39-1; 2,6-dichlorobiphenyl, 33146-45-1; 2,4,5-trichlorobiphenyl, 15862-07-4; 2,4,6-trichlorobiphenyl, 35693-92-6; 2,3,4,5-tetrachlorobiphenyl, 33264-53-6; 2,2',4',5'-tetrachlorobiphenyl, 41464-40-8; 2,3,4,5,6-pentachlorobiphenyl, 18259-05-7; 2,2',4,5,5'-pentachlorobiphenyl, 37680-73-2; 2,2',3,3',6,6'-hexachlorobiphenyl, 38411-22-2; 2,2',3,3',4,4'-hexachlorobiphenyl, 38380-07-3; 2,2',4,4',6,6'-hexachlorobiphenyl, 33979-03-2; 2,2',3,3',4,4',6-heptachlorobiphenyl, 52663-71-5; 2,2',3,3',5,5',6,6'-octachlorobiphenyl, 2136-99-4; 2,2',3,3',4,4',5,5',6,6'-nonachlorobiphenyl, 52663-77-1; 2,2',3,3',4,4',5,5',6,6'-decachlorobiphenyl, 2051-24-3.

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## Solubility of Uranium Hexafluoride in Some Low-Temperature Solvents

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The solubility of  $UF_6$  has been measured in several liquefied gases. Phosgene, nitrous oxide, and sulfur dioxide are found to be good solvents for  $UF_6$  at temperatures below  $0^\circ C$ . The results are compared with ideal and regular solution theory. Regular solution theory provides a reasonably good description of the  $UF_6/COCl_2$  system but is less good for the  $UF_6/SO_2$  system.

### Introduction

The solubility of uranium hexafluoride ( $UF_6$ ) in liquids has been studied many times, particularly in halocarbons (1-3) and fluorinated halogens (4-8). A few of these studies have included temperatures below  $0^\circ C$  (2, 5, 7) but there has been more interest in the solubilities at temperatures above  $0^\circ C$ .

It is the purpose of this paper to report the solubilities of  $UF_6$  in liquefied gases of small, inorganic molecules. Solubilities have been measured for temperatures between about 160 and 270 K, and the experimental observations are compared with regular solution theory.

### Experimental Methods

The apparatus is a calibrated, 80-mL, graduated, cylindrical, borosilicate glass flask measuring about 4 cm in diameter by 8 cm high and attached to a vacuum system through a glass

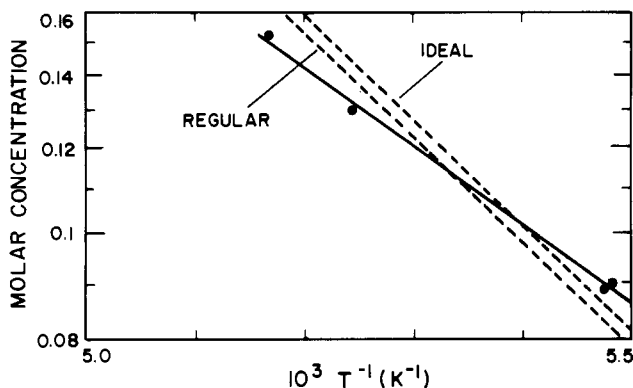
tube. The flask is surrounded by a clear glass Dewar, and the top of the Dewar is closed with a Styrofoam plug that fits around the vacuum line. A glass-encapsulated magnetic stirring rod is inside the flask. An iron-constantan thermocouple is inserted into a thin-walled glass well that protrudes into the interior of the flask; this thermocouple well is fused to the top of the flask and reaches nearly to the bottom.

The experimental procedure is as follows. The flask is evacuated to about  $10^{-4}$  torr and is heated to drive off any residual water. The bottom of the flask is then cooled with dry ice or liquid nitrogen, and the solute,  $UF_6$ , is condensed out from its gas phase. The Dewar is raised into position and closed with the Styrofoam plug. Further cooling of the flask is accomplished by blowing cold  $N_2$  gas into the Dewar through a hole in the Styrofoam plug. The solvent is condensed into the flask, and the mixture of  $UF_6$  and solvent is stirred vigorously. The temperature of the liquid is held constant, and solvent is slowly condensed into the flask in small increments. After each addition of solvent, the mixture is stirred for a period that depends on the solvent, the temperature, and the amount of undissolved  $UF_6$ . After most of the  $UF_6$  has been dissolved, solvent is added in very small increments and the stirring times between additions are lengthened, to ensure that the solution is saturated with  $UF_6$ . Some of the data points reported here have been obtained with a small fraction (<2%) of the total  $UF_6$  still undissolved. When the  $UF_6$  crystals just disappear under bright illumination, the stirring motion is stopped, and the level of the

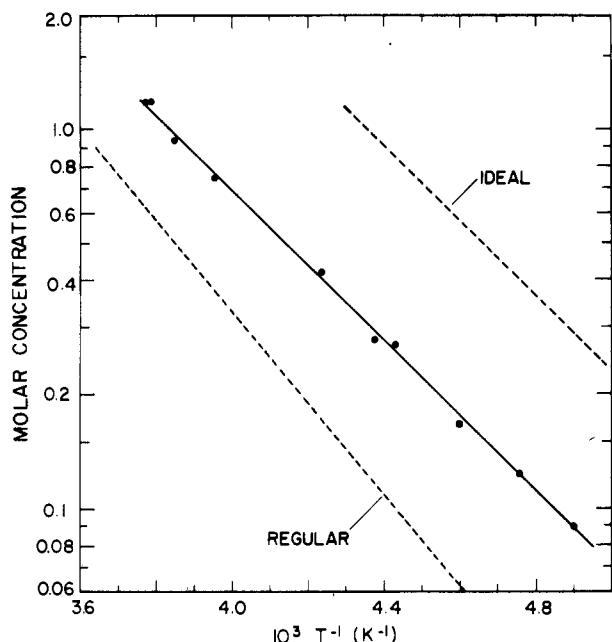
Table I. Solubilities and Some Remarks

solvent	temp, K	concn, <sup>a</sup> M	soln color	comments <sup>b</sup>	temp range, <sup>c</sup> K
COCl <sub>2</sub>	270.8	2.12	pale yellow <sup>d</sup>	slight residue	158.7-270.8
SO <sub>2</sub>	264.7	1.43	yellow <sup>d</sup>	slow reaction slight residue	203.9-264.7
N <sub>2</sub> O	193.7	0.185	colorless	no reaction	182.4-193.7
O <sub>2</sub>	77	<0.003 <sup>e</sup>	light blue <sup>f</sup>	residue	
H <sub>2</sub> S	223	<sup>e</sup>		reaction residue	
COS	205	<0.072 <sup>g</sup>	red-brown	reaction residue	

<sup>a</sup> This concentration is appropriate for the highest temperature at which the solubility was measured for a given solvent. <sup>b</sup> Residues sometimes remained after the solvent and all remaining UF<sub>6</sub> were pumped away. Reactions between UF<sub>6</sub> and the solvent (or some undetectable impurity in the solvent) were often observed. <sup>c</sup> Temperature ranges for which solubilities were measured. <sup>d</sup> The color depends on the concentration. <sup>e</sup> Insoluble, within the limitations of this experiment. <sup>f</sup> Pure O<sub>2</sub> is light blue. <sup>g</sup> Detailed measurements were not made on this system, but UF<sub>6</sub> did dissolve.



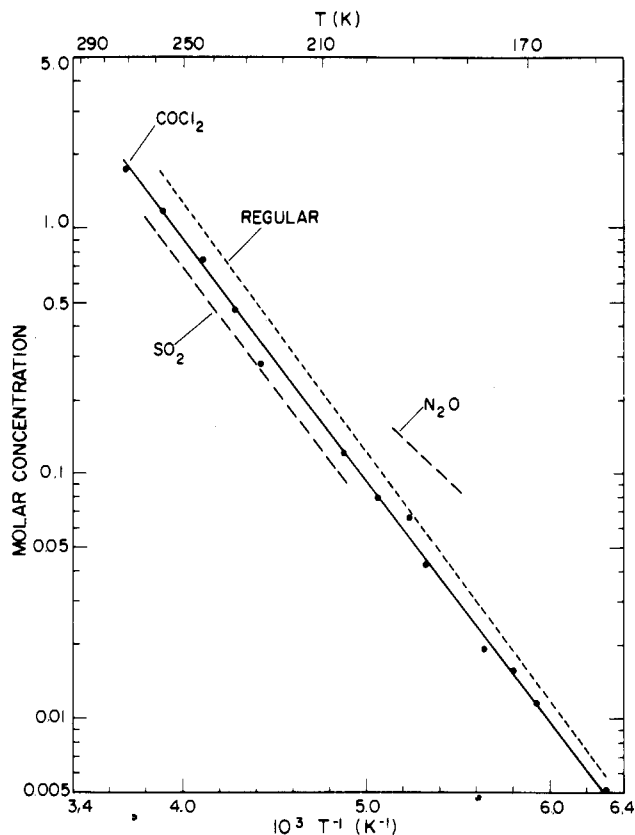
**Figure 1.** Molar concentration (moles of solute per liter of solution) of UF<sub>6</sub> in liquid N<sub>2</sub>O at saturation vs.  $10^3/T$ . Data are shown as solid circles (●). The solid line is judged to be an adequate representation of the data. The dashed lines are theoretical predictions of the solubility of UF<sub>6</sub> in liquid N<sub>2</sub>O.



**Figure 2.** Molar concentration of UF<sub>6</sub> in liquid SO<sub>2</sub> at saturation vs.  $10^3/T$ . The solid line is judged to be an adequate representation of the data (●). The dashed lines are theoretical predictions of the solubility of UF<sub>6</sub> in SO<sub>2</sub>.

solution within the flask is read.

The gases used in this experiment were the best, commercially available grade. Mass-spectral analyses were made of all gases. Before the COCl<sub>2</sub> was used, it was passed through a trap filled with MgO to remove a small HCl impurity. The UF<sub>6</sub>



**Figure 3.** Molar concentration of UF<sub>6</sub> in liquid COCl<sub>2</sub> at saturation vs.  $10^3/T$ . The solid line is judged to be an adequate representation of the data (●). The long-dashed lines are experimental solubilities reproduced from Figures 1 and 2 for comparison. The short-dashed line is the solubility predicted by regular solution theory for UF<sub>6</sub>/COCl<sub>2</sub>.

used was obtained from the Oak Ridge Gaseous Diffusion Plant and was better than 99.9% pure; our infrared analyses of the UF<sub>6</sub> revealed no impurities.

Temperatures quoted herein should be accurate to  $\pm 0.5$  °C. The total uncertainty in the volume measurements is  $\pm 3\%$ . The amount of UF<sub>6</sub> condensed into the flask is known within  $\pm 3\%$ , and at least 98% of the UF<sub>6</sub> has gone into solution for any data point. The maximum possible errors in the concentrations reported here should thus be  $\pm 8\%$ , and the reproducibility of the data should be about  $\pm 5\%$ .

## Results and Discussion

The liquefied gases used in this investigation are given in Table I, together with some experimental observations. UF<sub>6</sub> has been dissolved in N<sub>2</sub>O, COCl<sub>2</sub>, SO<sub>2</sub>, and COS. The COS solution was red-brown, and the UF<sub>6</sub> may have been dissolved

Table II. Solubility of UF<sub>6</sub>

T, K	concn, mol/L	T, K	concn, mol/L
COCl <sub>2</sub> as Solvent			
158.7	0.00502	197.7	0.0802
158.7	0.00508	205.0	0.122
168.7	0.0116	226.0	0.282
169.5	0.0152	233.2	0.467
169.5	0.0156	243.4	0.737
177.2	0.0193	256.8	1.17
187.7	0.0428	270.8	1.73
191.2	0.0670		
SO <sub>2</sub> as Solvent			
203.9	0.0894	235.8	0.415
210.2	0.123	252.2	0.755
217.2	0.166	259.4	0.950
225.6	0.267	263.7	1.18
228.2	0.278	264.7	1.18
N <sub>2</sub> O as Solvent			
182.4	0.0896	190.7	0.130
182.7	0.0886	193.7	0.152

as U(V), which has a characteristic reddish color.

The solubilities of UF<sub>6</sub> in liquid N<sub>2</sub>O, SO<sub>2</sub>, and COCl<sub>2</sub> have been measured over as wide a temperature range as possible with our apparatus. The data are presented in Figures 1–3 and in Table II. There are too few data points for N<sub>2</sub>O to be sure that the appropriate curve is indeed straight, but the solubilities of UF<sub>6</sub> in COCl<sub>2</sub> and SO<sub>2</sub>, when plotted against 1/T, lie along straight lines over a fairly wide range of temperatures.

The other lines shown in Figures 1–3 have been computed from regular or ideal solution theory for comparison with the data (9, 10). The equations used for regular solution theory are

$$RT \ln (a_2/x_2) = V_2 \phi^2 (\delta_1 - \delta_2)^2$$

$$\phi = x_1 V_1 / (x_1 V_1 + x_2 V_2)$$

$$\delta_k = [(\Delta H_k^v - RT) / V_k]^{1/2}$$

$$\ln a_2 = (\Delta H_0^f / R)(1/T_0 - 1/T) \quad (1)$$

For ideal solutions,  $\delta_1 - \delta_2 = 0$ . The numerals 1 and 2 label quantities appropriate for solvent and solute (UF<sub>6</sub>), respectively.  $T \equiv$  temperature in Kelvin.  $x_k \equiv$  mole fraction of component  $k$  in solution.  $R \equiv 1.988$  cal/(cm mol K).  $V_1 \equiv$  molar volume of the solvent.  $V_2 \equiv$  molar volume of the (hypothetical) liquid solute.  $\Delta H_k^v \equiv$  heat of vaporization of component  $k$ .  $T_0$  and  $\Delta H_0^f$  are respectively the melting point of the solute and the heat of fusion of the solute at  $T_0$ . Table III lists values used for the parameters appearing in these equations. Note that solutions of UF<sub>6</sub> in COCl<sub>2</sub> and in N<sub>2</sub>O are expected to be nearly ideal.

We have assumed that the difference,  $\Delta C_p$ , between the heat capacities of the liquid and solid solute are zero; in fact (8), for UF<sub>6</sub>,  $\Delta C_p \approx 2.1$  cal/(mol K) at the melting point of UF<sub>6</sub>. Since  $\Delta C_p \neq 0$ , the plot of  $\ln x_2$  against  $T^{-1}$  should be curved,

Table III. Heats of Fusion ( $\Delta H_0^f$ ), Heats of Vaporization ( $\Delta H^v$ ), Molecular Weight ( $M_r$ ), Molar Volumes ( $V_i$ ), and Solubility Parameters ( $\delta_i$ ) Evaluated at  $T = 200$  K

molecule	$\Delta H_0^f$ , kcal/mol	$\Delta H^v$ , kcal/mol	$M_r$	$V_i$ , cm <sup>3</sup>	$\delta$ , cal <sup>1/2</sup> cm <sup>-3/2</sup>
UF <sub>6</sub>	4.587 <sup>a</sup>	7.61 <sup>b</sup>	352.03	84.42 <sup>c</sup>	9.24
COCl <sub>2</sub>		6.80 <sup>d</sup>	98.91	61.62 <sup>e</sup>	10.19
SO <sub>2</sub>		6.70 <sup>f</sup>	64.06	39.74 <sup>e</sup>	12.63
N <sub>2</sub> O		3.77 <sup>g</sup>	44.01	35.91 <sup>e</sup>	9.70

<sup>a</sup> Taken from ref 11. <sup>b</sup> Obtained by subtracting the heat of fusion, 4.587 kcal, from the heat of sublimation, 12.20 kcal (p 423, ref 8) at 200 K. <sup>c</sup> Computed from the equation for the density in ref 12. <sup>d</sup> Obtained from data in ref 13 and from ref 11. <sup>e</sup> Computed from formulas and densities in ref 14. <sup>f</sup> Estimated by extrapolating the data in ref 15. <sup>g</sup> Taken from ref 15.

but for us to discern this curvature experimentally  $\Delta C_p \geq 8$  cal/(mol K) would be required. The curvature arising from finite  $\Delta C_p$  will not, therefore, be observable in our data. The term involving  $\Delta C_p$  is small ( $\sim 20$  cal/mol at 200 K) compared with  $\Delta H_0^f$  ( $\sim 4500$  cal/mol) and has been taken to be zero.

For comparison of the calculated and experimental curves, we have estimated effects caused by variation of solvent density with temperature, and we have found the effect to be negligible. Similarly, we have calculated the number density,  $n_2$ , of the dissolved UF<sub>6</sub> from  $n_2 = V_1/x_2$ , and we find that this assumption should cause the calculated curves for  $n_2$  to be  $\sim 3\%$  higher than the observed solubility of UF<sub>6</sub> in COCl<sub>2</sub> at 270 K; the effect of this assumption is negligible for all other data points.

The slopes of the lines computed from regular solution theory and plotted in Figures 2 and 3 are very similar to the slopes of the lines representing the observations over the temperature range for which we have data. The absolute solubilities of UF<sub>6</sub> in SO<sub>2</sub> and COCl<sub>2</sub> are not within estimated experimental error of the theoretical curves. Regular solution theory provides a fairly good ( $\sim 30\%$ ) quantitative estimate of the solubility of UF<sub>6</sub> in COCl<sub>2</sub> between 158 and 275 K but predicts that the concentration of UF<sub>6</sub> in SO<sub>2</sub> will be a factor of 2–3 below observed values.

In Figure 1, the measured and predicted absolute solubilities of UF<sub>6</sub> in N<sub>2</sub>O agree fairly well, but the slope of the curve representing the observed solubilities differs significantly from the slope of the theoretical curve. The significance of this difference in slopes is hard to assess from our data, because the temperature range of our observations is small and the difference in slopes is not very far outside of the range of estimated uncertainty. Regular solution theory provides a reasonably good (5–10%) estimate of the solubility in UF<sub>6</sub> in N<sub>2</sub>O between 182 and 194 K.

Regular solution theory does not represent any of the present binary systems within the estimated experimental uncertainty, but the comparison of theory and experiment may be invalidated by several things. First, values estimated for the solubility parameters depend in some cases on extrapolations which may be in error. In the case of UF<sub>6</sub>/N<sub>2</sub>O, uncertainties in our data may contribute significantly to the lack of agreement. Finally, the solubility parameters are estimated at 200 K, and somewhat different theoretical curves will, in practice, result if the solubility parameters are evaluated at some other temperature. We conclude that, at least for UF<sub>6</sub>/N<sub>2</sub>O and UF<sub>6</sub>/COCl<sub>2</sub>, the differences between the theory and the experiment may not be significant.

## Conclusions

Liquid COCl<sub>2</sub>, SO<sub>2</sub>, N<sub>2</sub>O, and even COS are all reasonably good solvents for UF<sub>6</sub>. Regular solution theory adequately represents our data for the solubility of UF<sub>6</sub> in N<sub>2</sub>O and COCl<sub>2</sub> but is less good for the solubility of UF<sub>6</sub> in SO<sub>2</sub>. Although our temperatures are lower than in some previous investigations, it appears that the liquids studied here are better solvents for

UF<sub>6</sub> than many of the halocarbons and fluorinated halogens studied in the past (1, 4). Thus, reasonably good, low-temperature solvents exist for uranium hexafluoride, even among rather simple solvent molecules.

**Registry No.** UF<sub>6</sub>, 7783-81-5; COCl<sub>2</sub>, 75-44-5; N<sub>2</sub>O, 10024-97-2; SO<sub>2</sub>, 7446-09-5.

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## Heat Capacities of Some Binary and Ternary Aqueous Nonelectrolyte Systems

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Heat capacities of a variety of binary and ternary aqueous nonelectrolyte systems were measured and the data fitted to  $C_{p,\phi} = C_{p,\phi}^{\circ} + c_2m + c_3m^2$ . The systems studied were aqueous solutions of acetamide, acetone, *p*-dioxane, dimethylformamide, ethyl acetate, formamide, hexamethylenetetramine, methyl formate, *s*-trioxane, and combinations of two of the above solutes. Internal consistency of data is very good and  $c_2$  coefficients agree with literature values. However, small discrepancies of  $C_{p,\phi}^{\circ}$  with literature values are observed, indicating a problem with the calorimeter.

#### Introduction

Heat capacities of binary and ternary aqueous solutions of myoinositol (IN), D-mannitol (MAN), cyclohexanol (CHEX), formamide (F), *N,N*-dimethylformamide (DMF), *s*-trioxane (T), and hexamethylenetetramine (HMT) were measured to complement recent enthalpy studies (1-5). Heat capacity measurements contribute to an understanding of solutions: details of structural effects have been found (6, 7), solute-solvent and solute-solute interactions have been uncovered (8-12), evidence of pseudophase transitions in binary aqueous organic systems (13) has been cited, and means have been provided for evaluating both the temperature dependence of excess thermodynamic properties (14) and isothermal compressibilities from isentropic compressibilities (15).

Much of the interest in heat capacity measurements has arisen in the past decade as a result of the widespread use of flow calorimeters, particularly those of the Picker type (16). Flow calorimetry offers a number of advantages over earlier techniques: higher sensitivity, elimination of vapor-space cor-

rections, short response times, small sample size, and rapid collection of data. These inherent advantages, together with some elegant design features, make possible the use of "the general principle that it is preferable to measure heat capacities as a function of temperature and integrate to obtain enthalpies at various temperatures than to derive heat capacities from the temperature dependence of enthalpies" (15). This type of calorimeter is now being used for measurements at high temperatures (17-23). With the great importance now attached to heat capacity measurements, it is essential that the accuracy of the data should not be called into question. The results presented here give rise to some concern over this matter.

#### Experimental Section

**Materials.** The purification of myoinositol (1), D-mannitol (1), cyclohexanol (1), formamide (2), *N,N*-dimethylformamide (2), *s*-trioxane (3), and hexamethylenetetramine (5) used by one of us (I.R.T.) has been previously reported. The purification of acetamide, acetone, dioxane, ethyl acetate, formamide, hexamethylenetetramine, D-mannitol, methyl formate, and *s*-trioxane (used by S.K.S.) has also been reported elsewhere (24). Details of solution preparation and handling are also available (1-3, 5).

**Apparatus and Procedure.** Measurements were taken with a Sodev Model CP-C Picker-type flow heat capacity microcalorimeter (16, 25, 26). Essentially, two liquids (1 and 2) with heat capacities per unit volume of  $\sigma_1$  and  $\sigma_2$  are maintained at the same temperature and flow rate as they enter twin cells; here they are simultaneously heated in such a manner that their final temperatures are identical. If  $W_1$  and  $W_2$  are the electrical powers supplied to produce the temperature rise, then, under ideal circumstances (i.e., no heat losses), we have

$$\frac{W_2 - W_1}{W_1} = \frac{\sigma_2 - \sigma_1}{\sigma_1} \quad (1)$$

The instrumentation is arranged so that the difference in applied

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